Mathematical Modeling of Chemical Processes Part II

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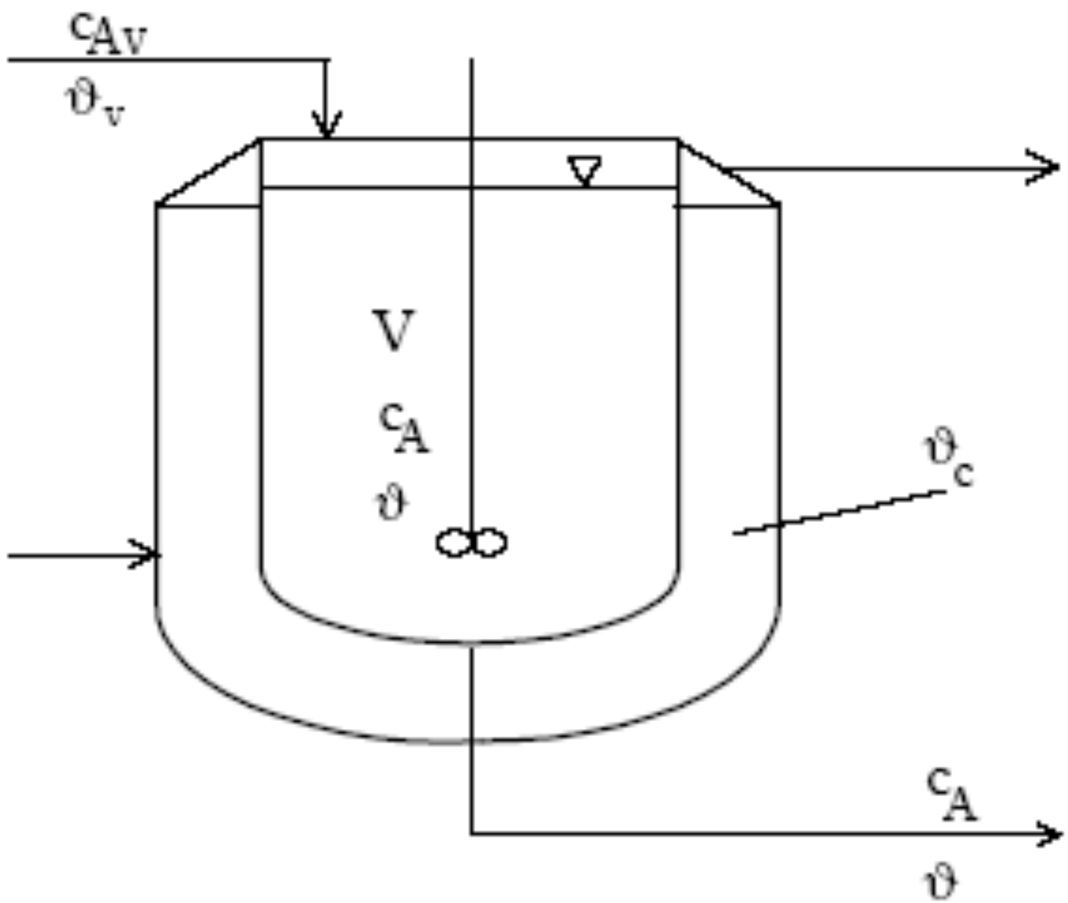
Continuous Stirred-Tank Reactor (CSTR)

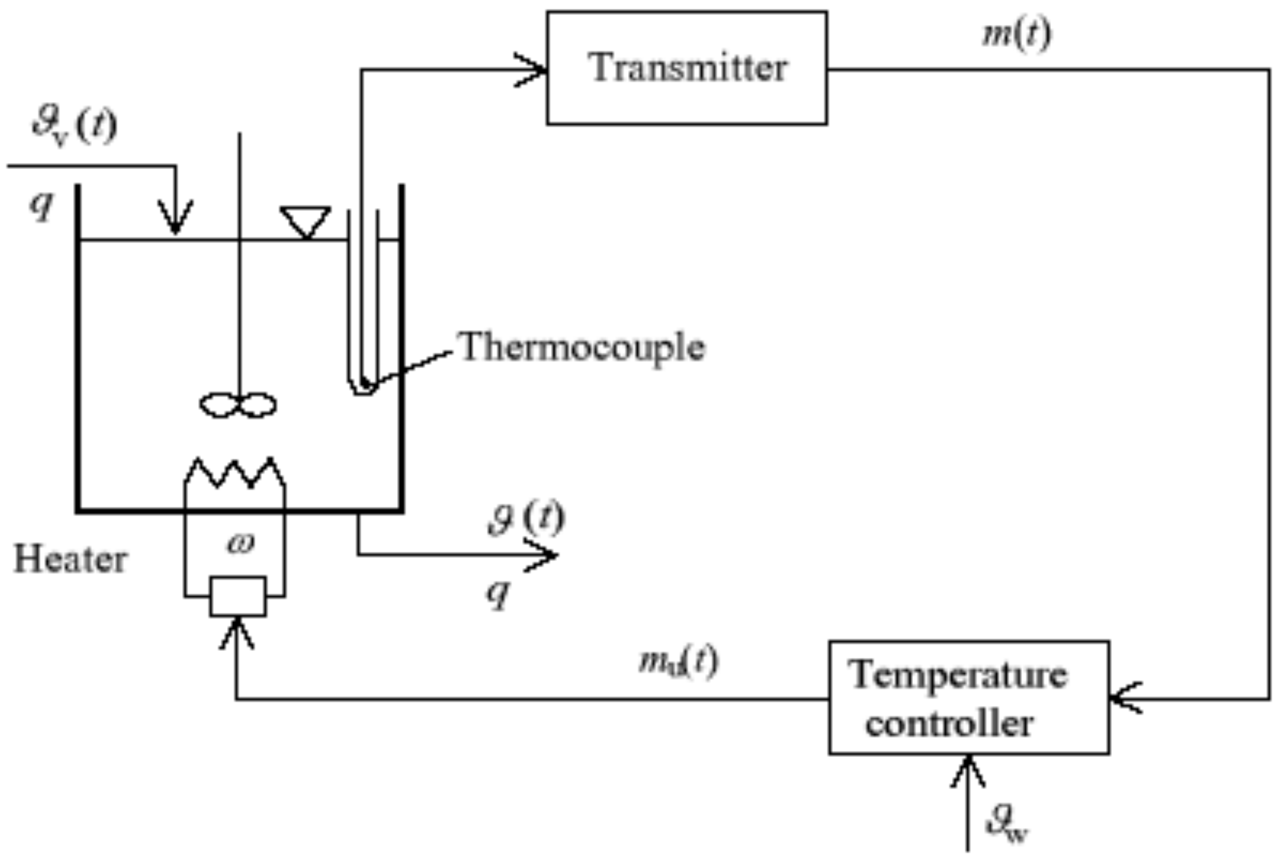


Continuous Stirred-Tank Reactor (CSTR)

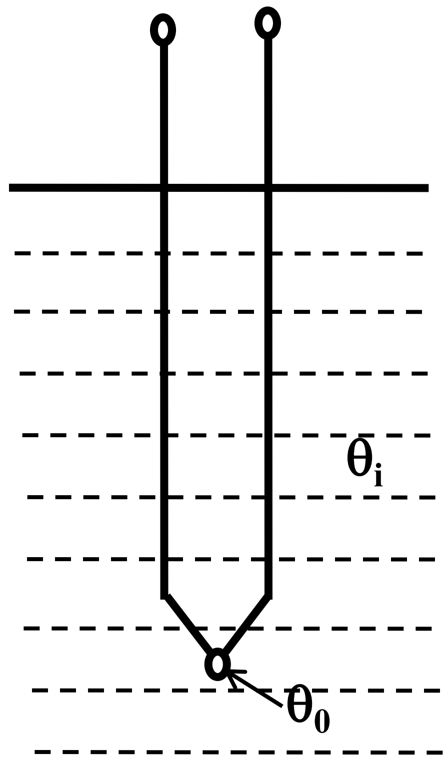
Assumptions

- neglected heat capacity of inner walls of the reactor, constant density and specific heat capacity of liquid,
- constant reactor volume, constant overall heat transfer coefficient, and
- constant and equal input and output volumetric flow rates.
- the reactor is well-mixed.

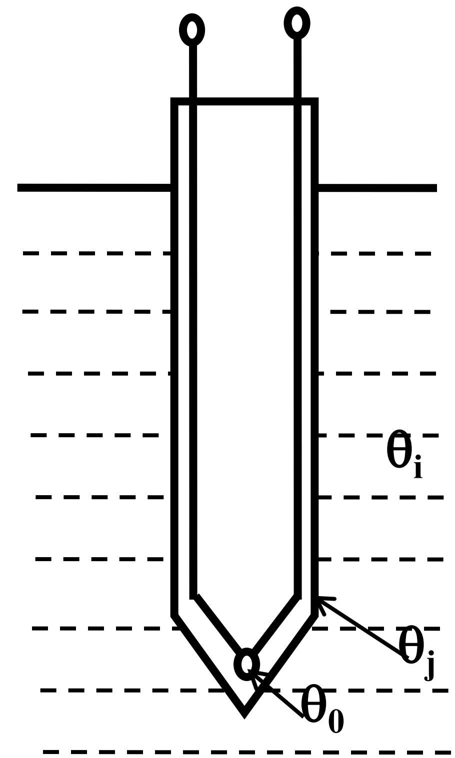
Control loop for the Stirred Heating Tank



Mathematical model of a thermocouple

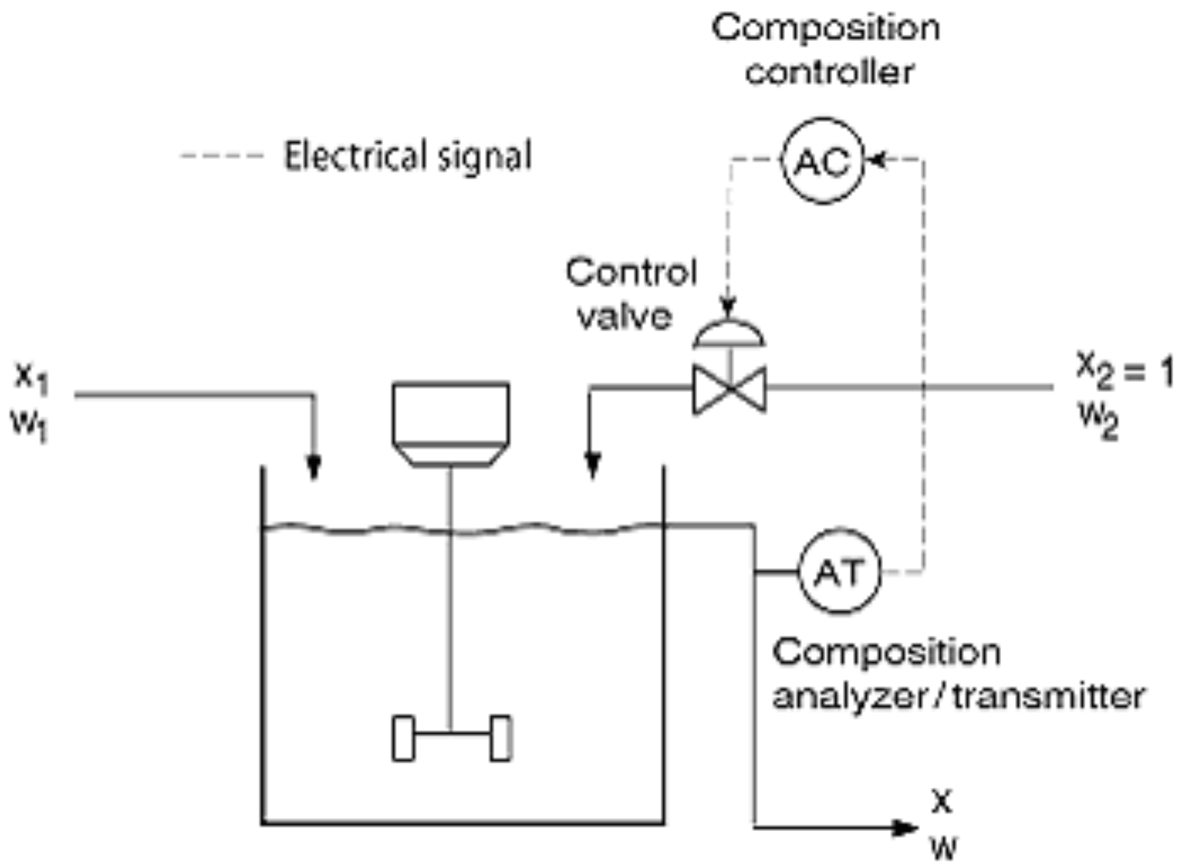


a) bare thermocouple

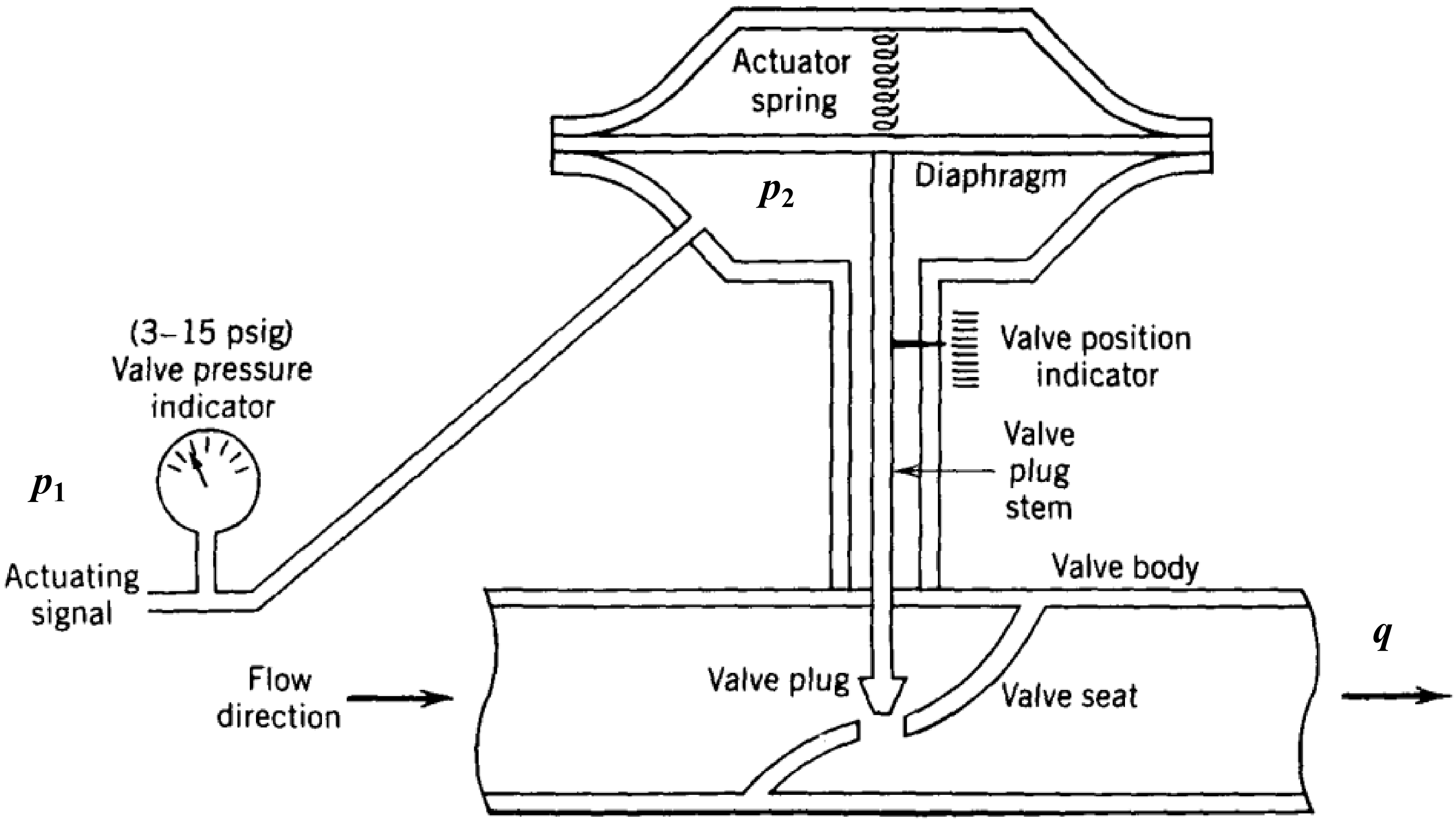


b) thermocouple with protect jacket

Blending system Control Method



Modeling the pneumatic control valve



Element Time Responses

- **first order element**

$$\tau \frac{dy(t)}{dt} + y(t) = Kx(t)$$

  - **Transfer function**

$$G(s) = \frac{Y(s)}{X(s)} = \frac{K}{\tau s + 1}$$

Element Time Responses

- **Step input *x*(*t*) = *MU*(*t*)**

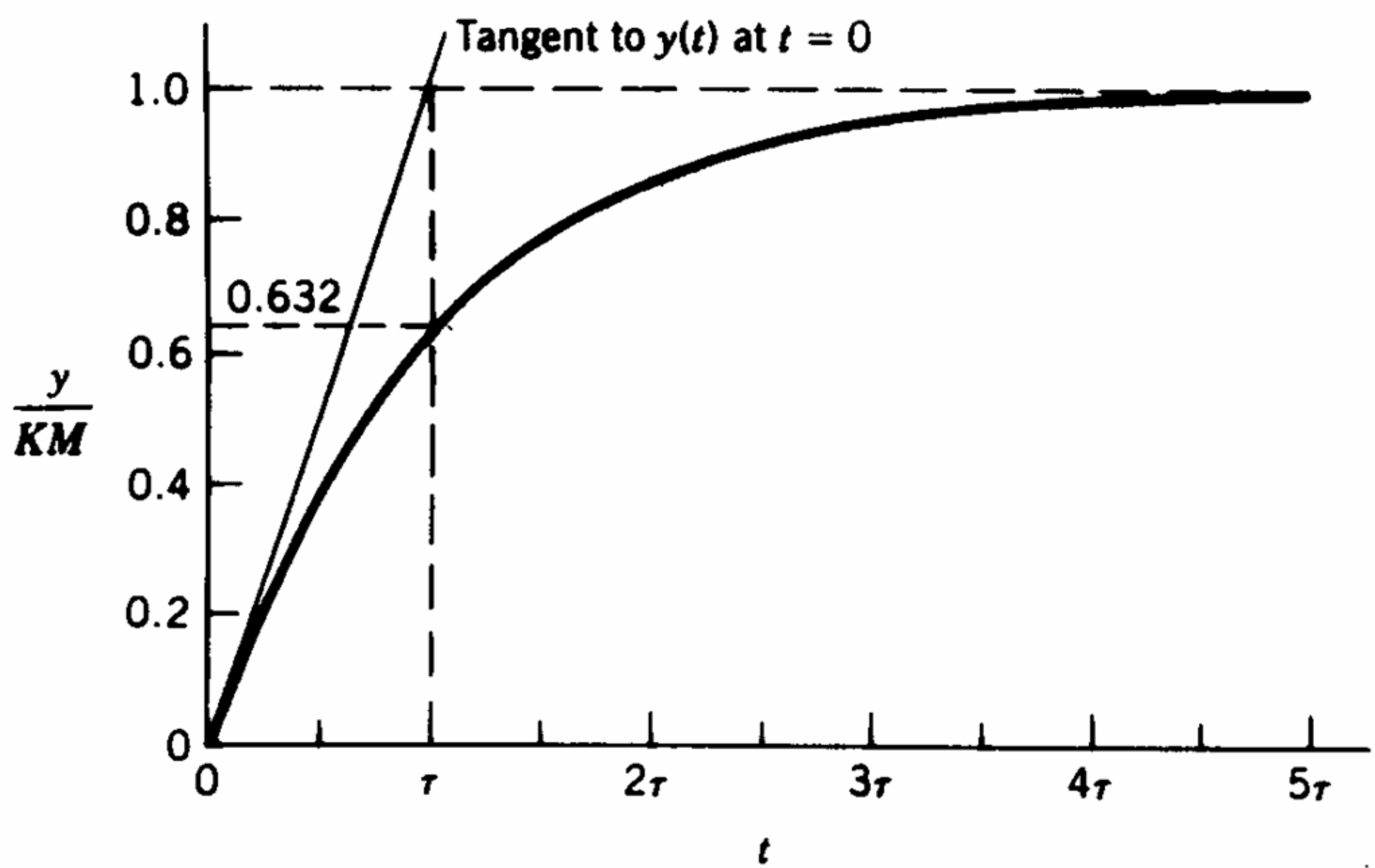
$$Y(s) = G(s)X(s) = \frac{K}{\tau s + 1} \cdot \frac{M}{s}$$

$$y(t) = \mathcal{L}^{-1}\left[\frac{K}{\tau s + 1} \cdot \frac{M}{s}\right] = KM\left(1 - e^{-\frac{t}{\tau}}\right)$$

  – **When *M* =1 (unit step input),**

$$y(t) = K\left(1 - e^{-\frac{t}{\tau}}\right)_{t=\tau} = 0.632$$

Element Time Responses



Element Time Responses

- **Second order element**

$$\tau_m^2 \frac{d^2 y(t)}{dt^2} + 2\zeta\tau_m \frac{dy(t)}{dt} + y(t) = x(t)$$

$$G(s) = \frac{Y(s)}{X(s)} = \frac{1}{\tau_m^2 s^2 + 2\zeta\tau_m s + 1}$$

$$= \frac{\omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2}$$

Second order element

- **Given a step input *x*(*t*) = *MU*(*t*),**

$$Y(s) = G(s)X(s) = \frac{\omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2} \cdot \frac{M}{s}$$

- **Use notations in Chapter 4, and let *M*=1 (unit step)**

$$C(s) = \frac{\omega_n^2}{s\left(s^2 + 2\zeta\omega_n s + \omega_n^2\right)}$$

Second order element

- **Factoring the denominator**

$$C(s) = \frac{\omega_n^2}{s\left(s + \zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1}\right)\left(s + \zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1}\right)}$$

- **Case A damping ratio equals unity ζ = 1**

$$C(s) = \frac{\omega_n^2}{s\left(s + \omega_n\right)^2}$$

Second order element

- **Partial fraction expansion**

$$C(s) = \frac{K_1}{s} + \frac{K_2}{\left(s+\omega_n\right)^2} + \frac{K_3}{\left(s+\omega_n\right)}$$

$$= \frac{1}{s} + \frac{-\omega_n}{\left(s+\omega_n\right)^2} + \frac{-1}{\left(s+\omega_n\right)}$$

- **The time domain responses of output**

$$c(t) = 1 - \omega_n t e^{-\omega_n t} - e^{-\omega_n t}$$

Second order element

- **Case B damping ratio greater than unity $\zeta > 1$**

$$C(s) = \frac{K_1}{s} + \frac{K_2}{\left(s + \zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1}\right)} + \frac{K_3}{\left(s + \zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1}\right)}$$

$$C(s) = \frac{1}{s} + \frac{\left[2\left(\zeta^2 - \zeta\sqrt{\zeta^2 - 1} - 1\right)\right]^{-1}}{\left(s + \zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1}\right)} + \frac{\left[2\left(\zeta^2 + \zeta\sqrt{\zeta^2 - 1} - 1\right)\right]^{-1}}{\left(s + \zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1}\right)}$$

Second order element

- **The time domain responses of output**

$$c(t) = 1 + \left[2\left(\zeta^2 - \zeta\sqrt{\zeta^2 - 1} - 1\right)\right]^{-1} e^{-\left(\zeta - \sqrt{\zeta^2 - 1}\right)\omega_n t}$$
$$+ \left[2\left(\zeta^2 + \zeta\sqrt{\zeta^2 - 1} - 1\right)\right]^{-1} e^{-\left(\zeta + \sqrt{\zeta^2 - 1}\right)\omega_n t}$$

- **Case C damping ratio less than unity ζ < 1**

Let $\zeta = \cos\alpha$, and therefore $\sqrt{1 - \zeta^2} = \sin\alpha$

Second order element

- **Partial fraction expansion**

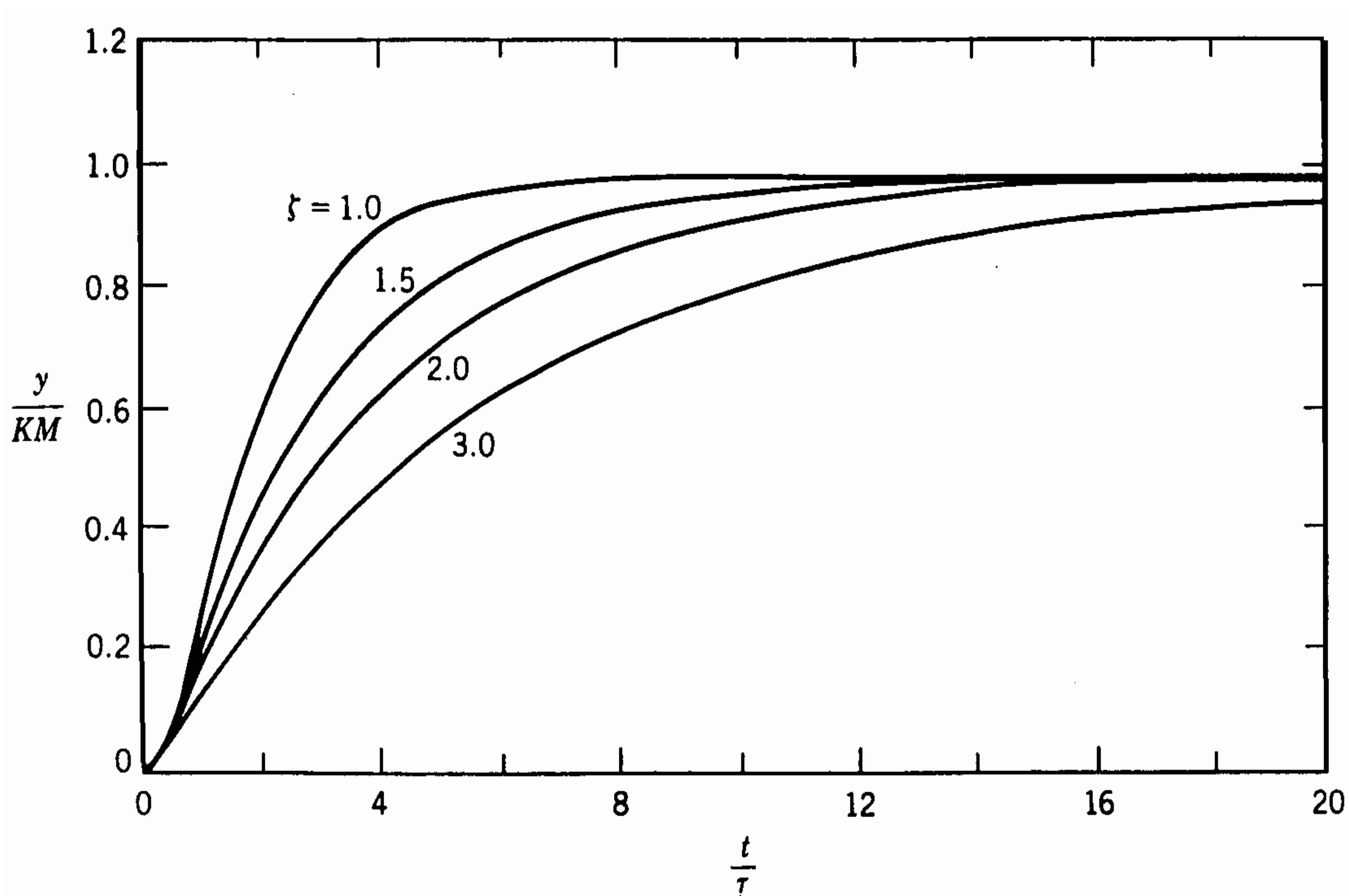
$$C(s)=\frac{1}{s}+\frac{e^{-j\alpha}}{2j\sin\alpha}\left(s+\zeta\omega_n-j\omega_n\sqrt{1-\zeta^2}\right)^{-1}$$

$$-\frac{e^{-j\alpha}}{2j\sin\alpha}\left(s+\zeta\omega_n+j\omega_n\sqrt{1-\zeta^2}\right)^{-1}$$

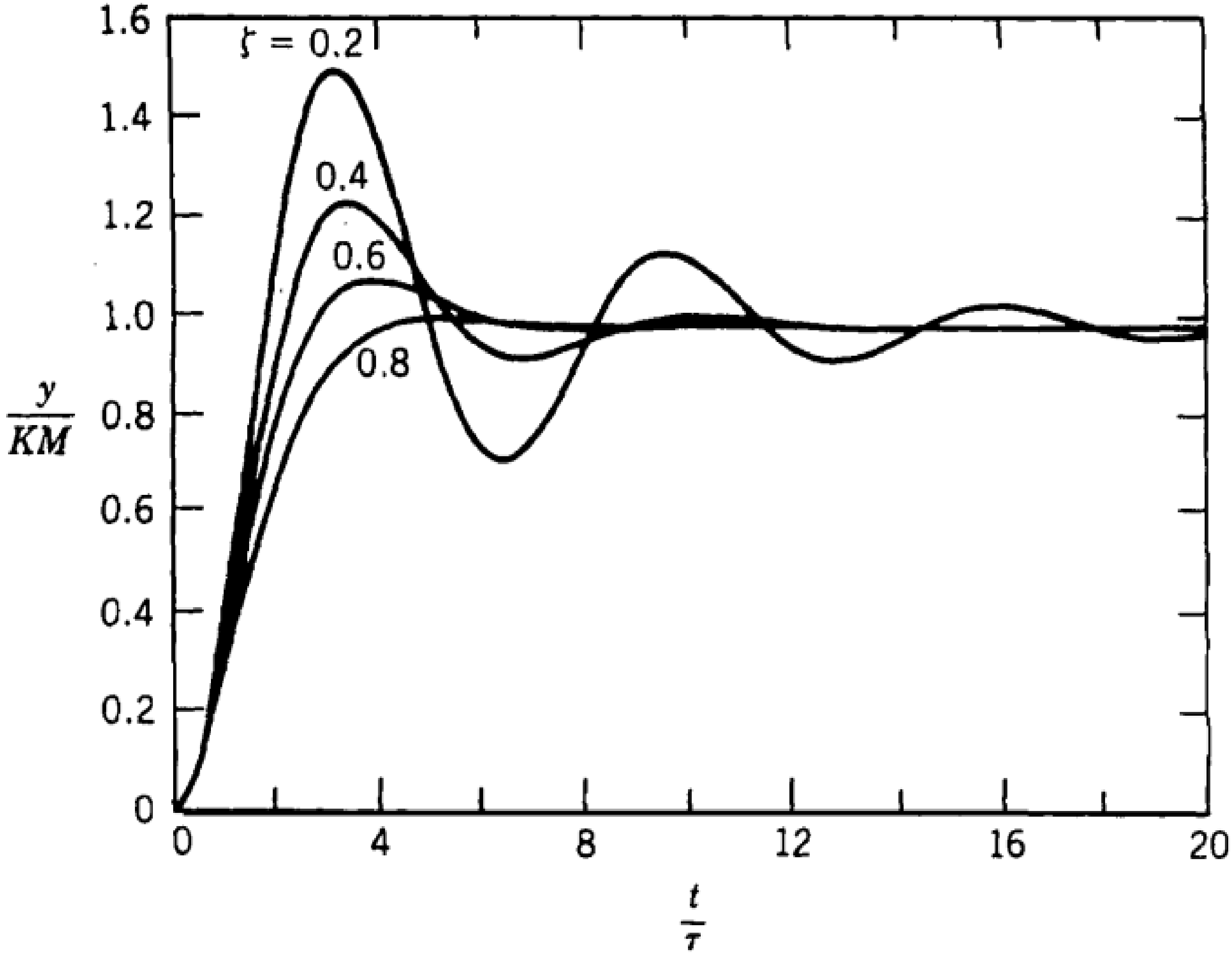
- **The time domain responses of output**

$$c(t)=1-\frac{e^{-\zeta\omega_n t}}{\sqrt{1-\zeta^2}}\sin\left(\omega_n\sqrt{1-\zeta^2}\,t+\alpha\right)$$

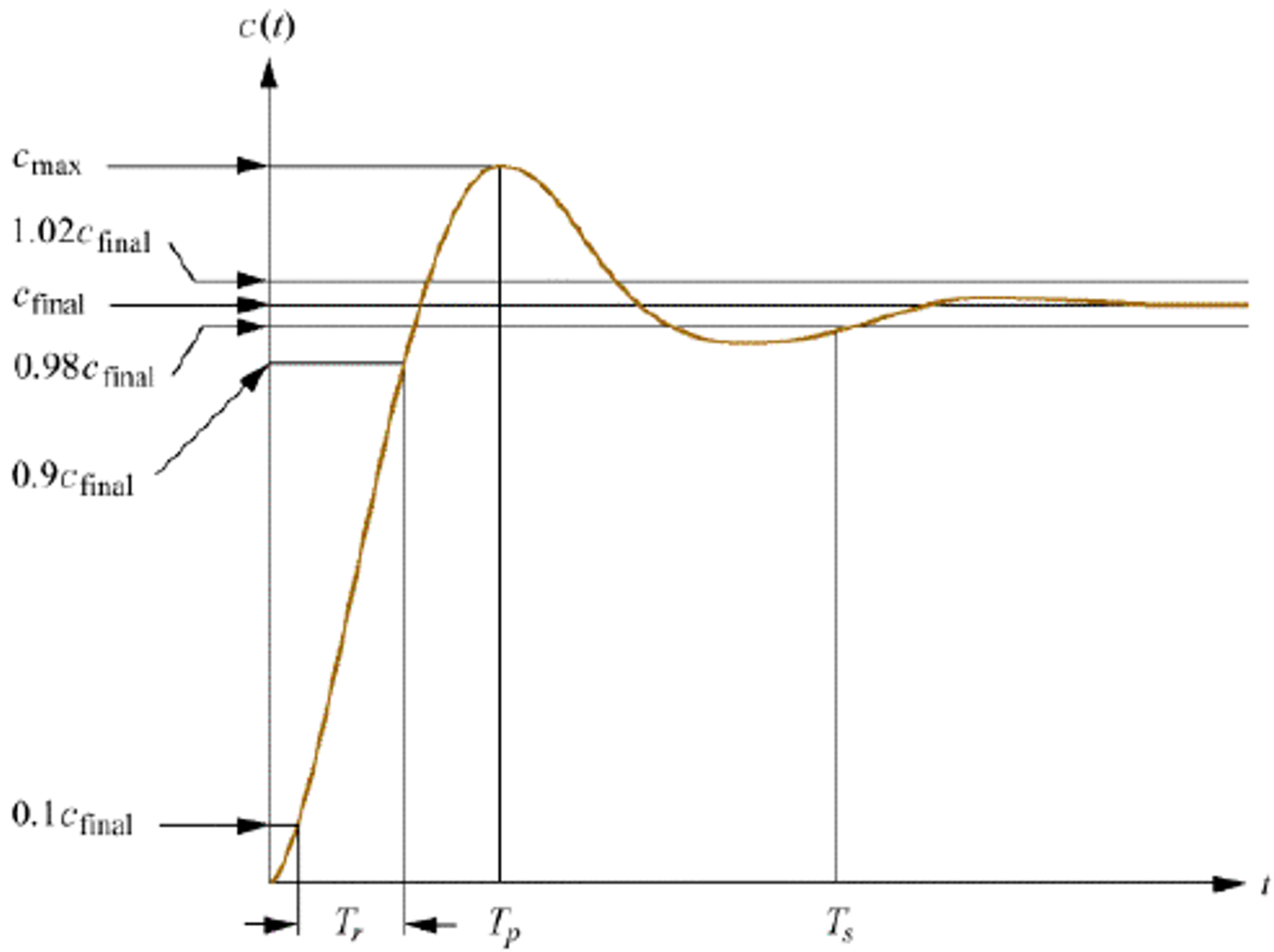
Step responses of a second order element over damped $\zeta \geq 1$



Step responses of a second order element under damped ζ<1



Second order underdamped response specifications



Performance specifications of a second-order system

- **Let**

$$\frac{dc(t)}{dt} = 0$$

- **We have**

$$\omega_n \sqrt{1-\zeta^2}\, t = 0, \pi, 2\pi \cdots$$

- **therefore**

$$c_{\max}(t) = 1 - \frac{e^{-\zeta\omega_n t}}{\sqrt{1-\zeta^2}} \sin(\pi + \alpha)$$

$$= 1 + \exp\left(\frac{-\zeta\pi}{\sqrt{1-\zeta^2}} \right)$$

Performance specifications of a second-order system

- **Peak time T_p, the time required to reach the first peak**

$$T_p = \frac{\pi}{\omega_n \sqrt{1-\zeta^2}}$$

- **Percent overshoot, %OS is the amount that the waveform overshoots the final steady-state**

$$\%OS = \exp\left(\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}\right)$$

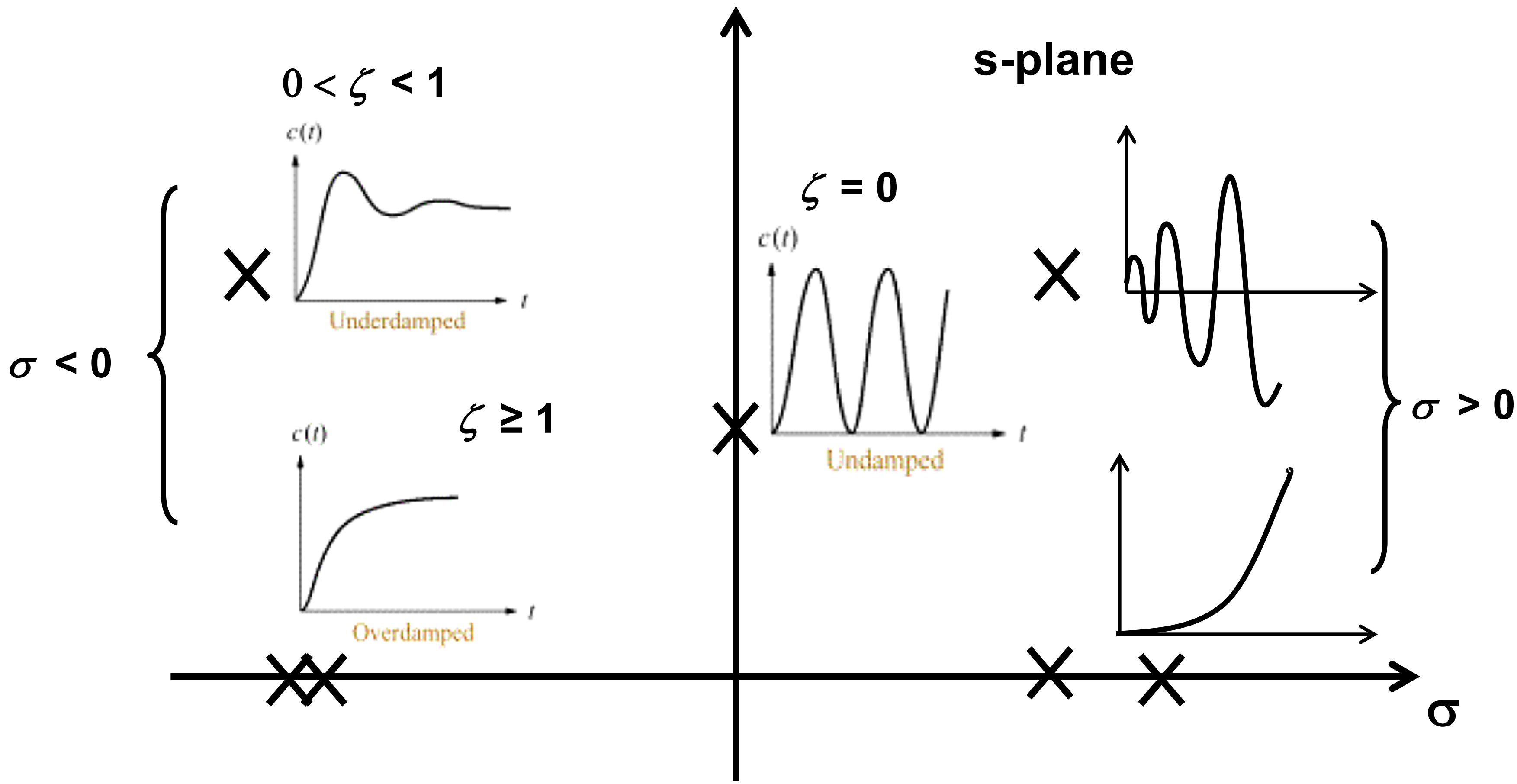
Performance specifications of a second-order system

- **Settling time T_s, the time required for damped oscillations to reach and stay within ±2% of the steady-state (final) value**

$$T_s = \frac{4}{\zeta \omega_n}$$

- **Rise time T_r is the time required for the waveform to go from 0.1 to 0.9 of the final value**

Location of the Roots in the s-plane and the Transient Response



Element Time Response

- **Proportional element**

  It is a step with *KM* as its magnitude

- **Integral element**

  It is a ramp at the slop of KM/τ_i

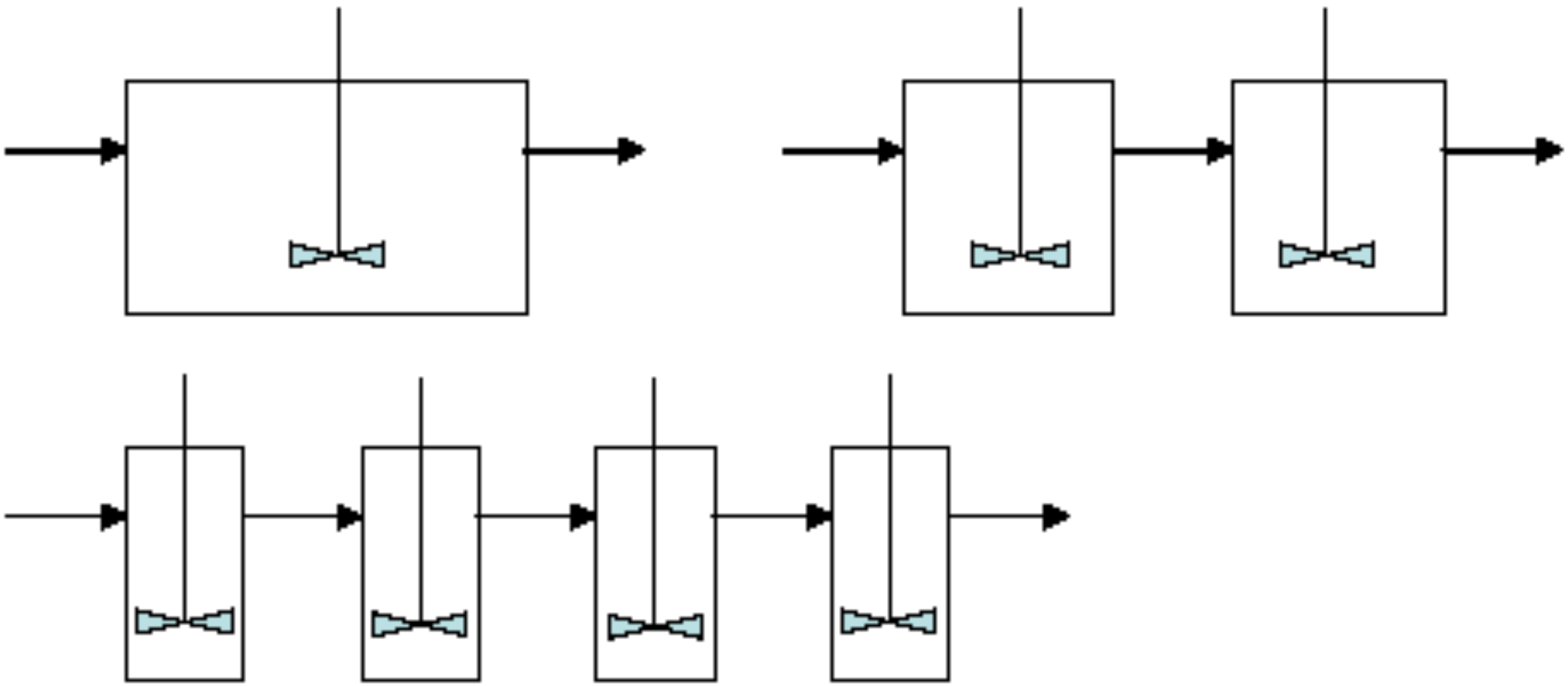
- **Differential element**

  It is a impulse

- **Delay element**

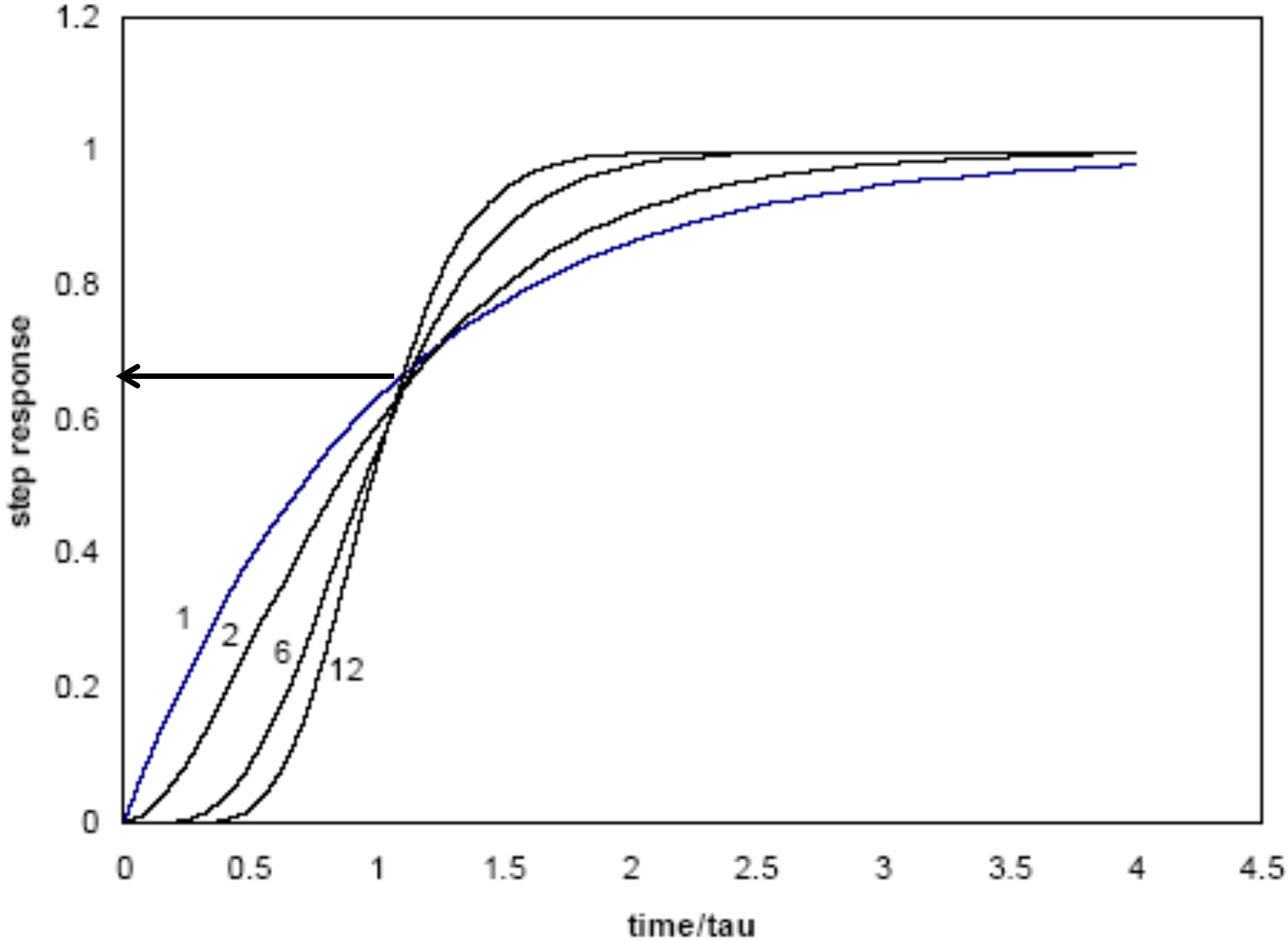
  It is a step after a time delay of τ

Development of Empirical Dynamic Models from Step Response Data



Higher order system and dead time

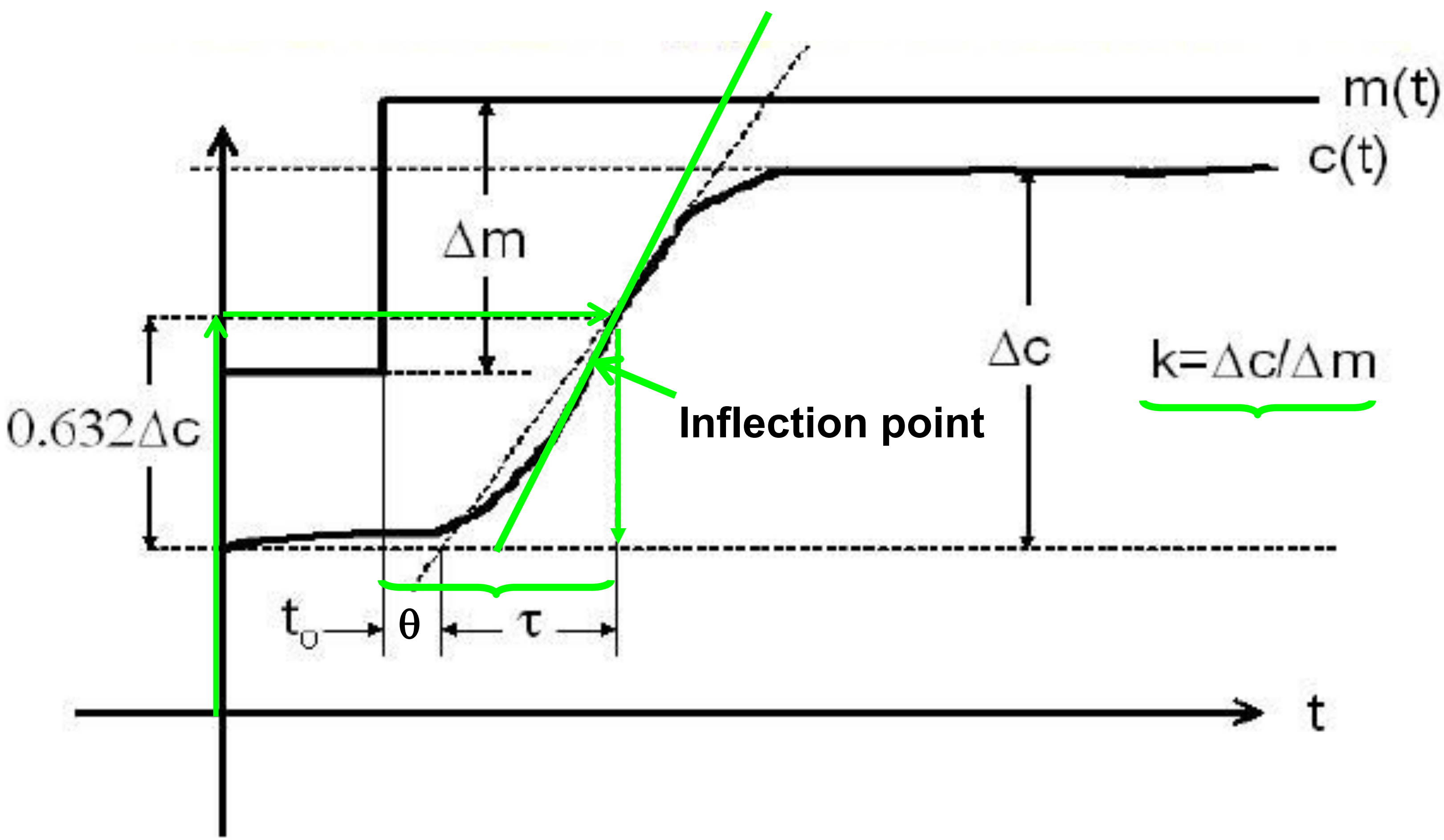
Higher order system and dead time



Approximate using first-order-plus-time-delay model

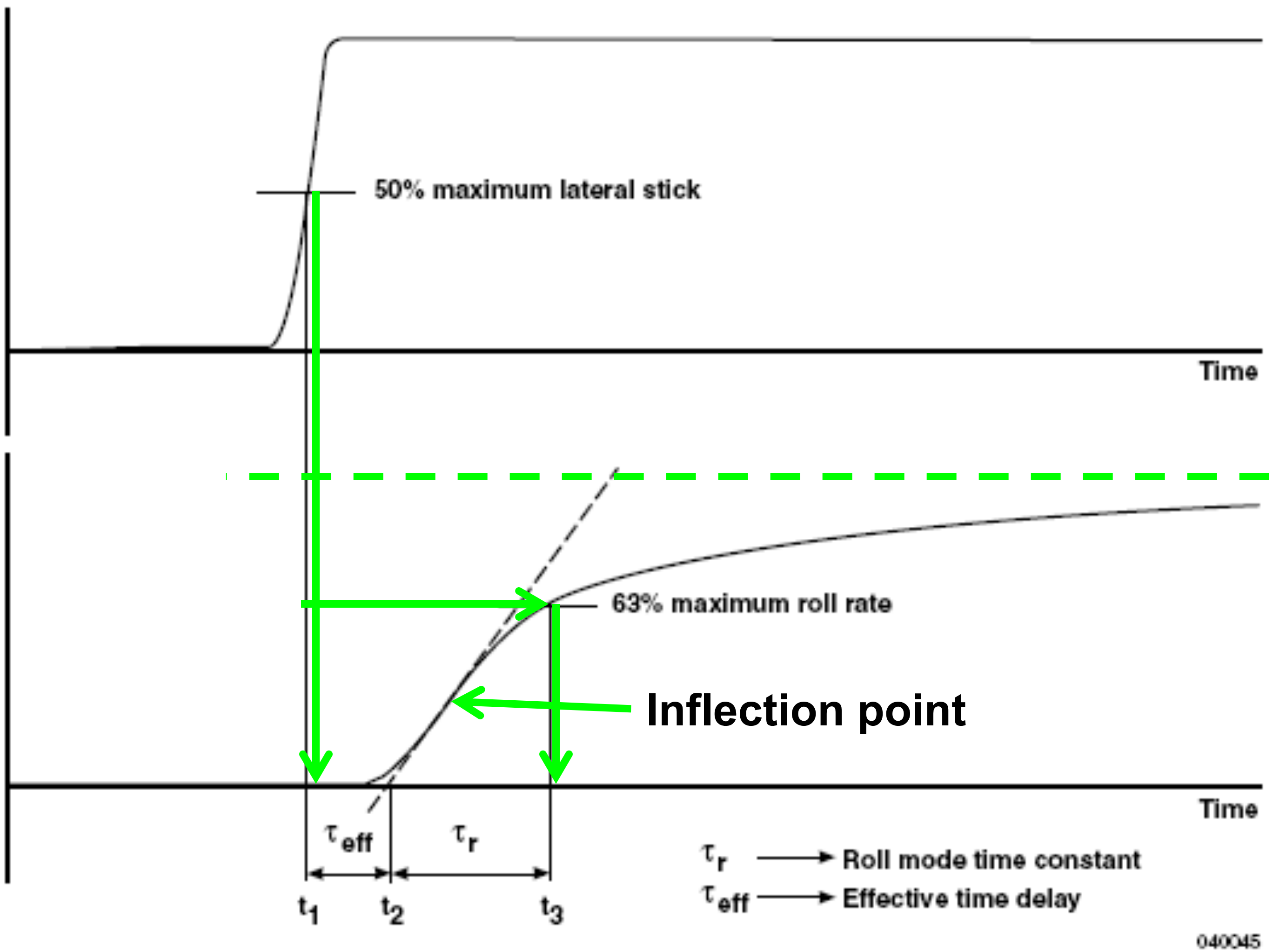
- **The response attains 63.2% of its final response at one time constant (*t* = $\tau + \theta$)**
- **The line drawn tangent to the response at maximum slope (*t* = θ) intersects the 100% line at (*t* = $\tau + \theta$).**
- **K is found from the steady state response for an input change magnitude *M*. The step response is essentially complete at *t* = 5τ.**

Approximate using first-order-plus-time-delay model

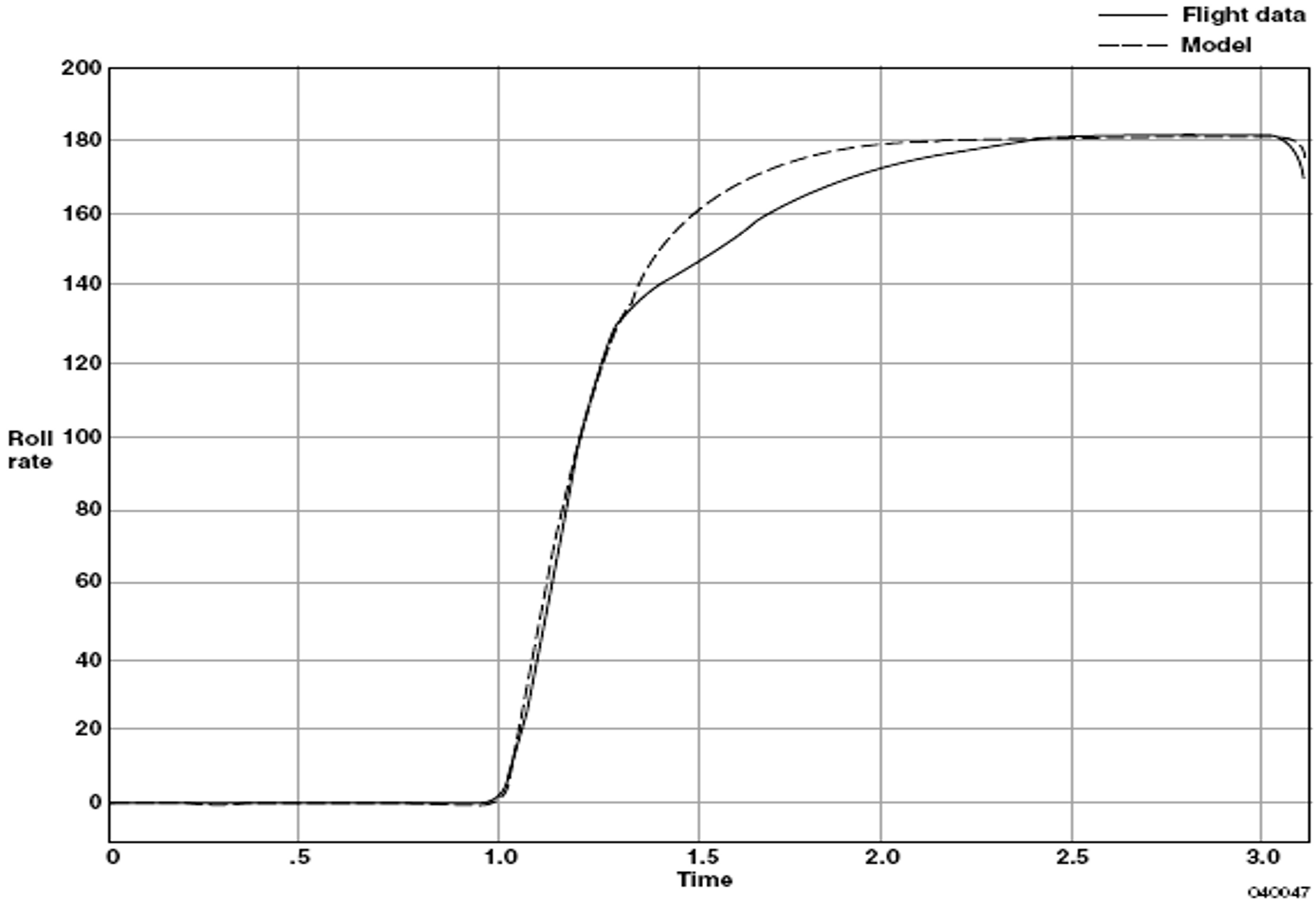


F-16XL Roll Mode Time Constant

F-16XL Roll Mode Time Constant



F-16XL Roll Mode Time Constant



Sundaresan and Krishnaswamy's

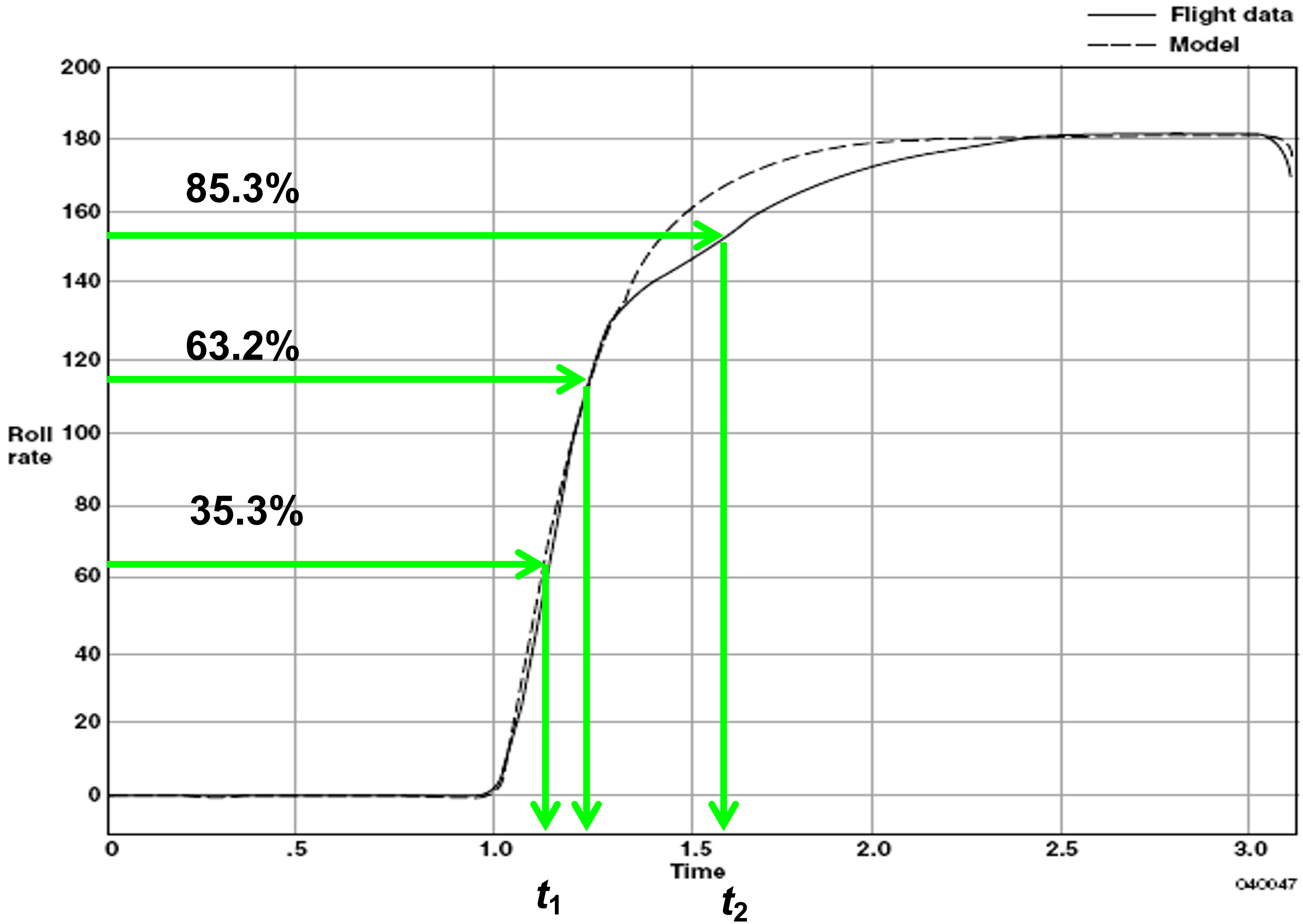
Inflection point of the process reaction curve is too arbitrary and difficult to determine when data is noisy

- **Step 1 take 35.3% response time t_1**
- **Step 2 take 85.3% response time t_2**
- **Substitute into the equations**

$$\theta = 1.3t_1 - 0.29t_2$$

$$\tau = 0.67\left(t_2 - t_1\right)$$

F-16XL Roll Mode Time Constant



Second-order Model

In general, a better approximation to an experimental step response can be obtained by fitting a second-order model to the data

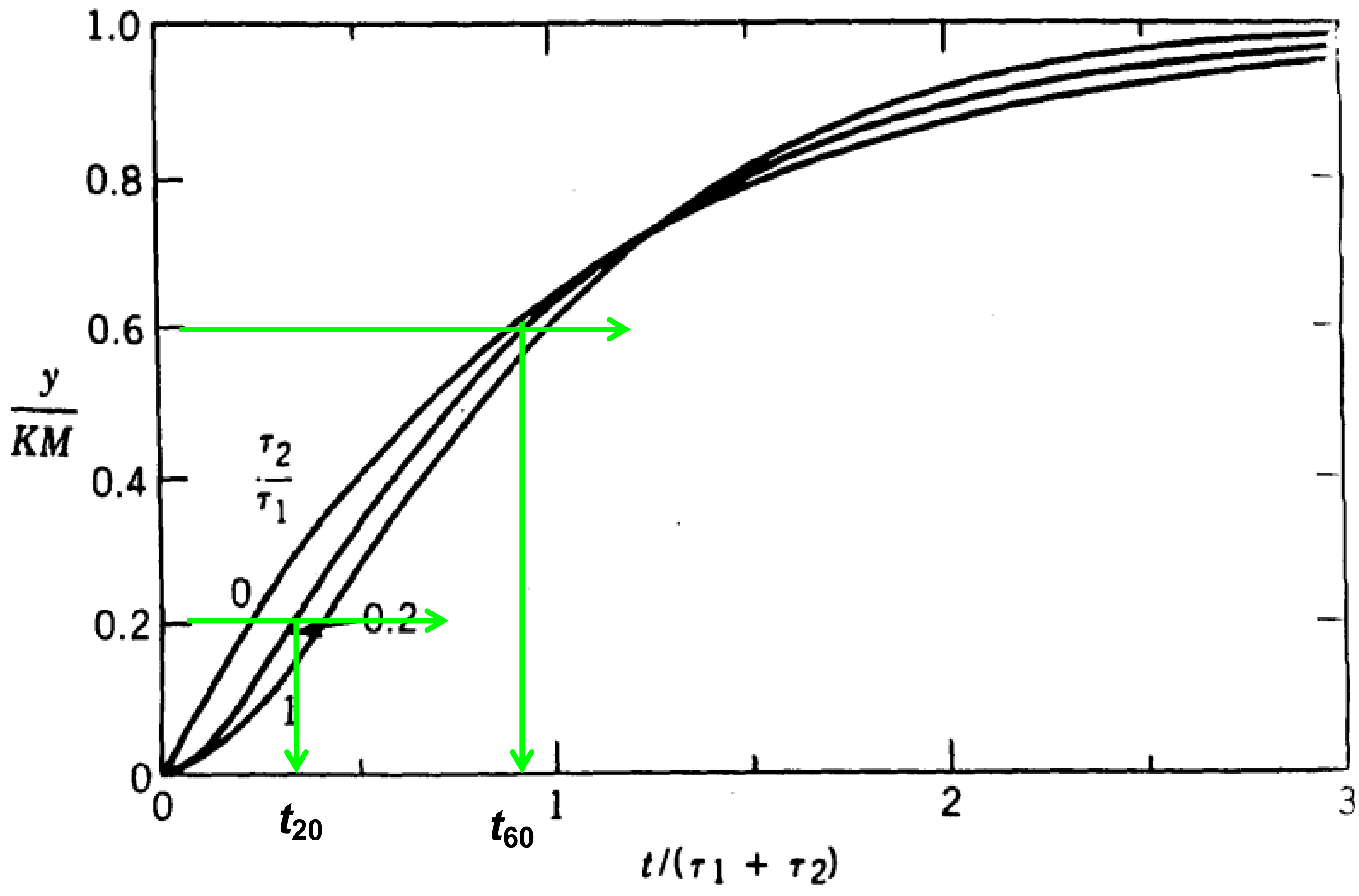
$$G(s) = \frac{K}{(\tau_1 s + 1)(\tau_2 s + 1)}$$

The larger of the two time constants, τ_1, is called the dominant time constant

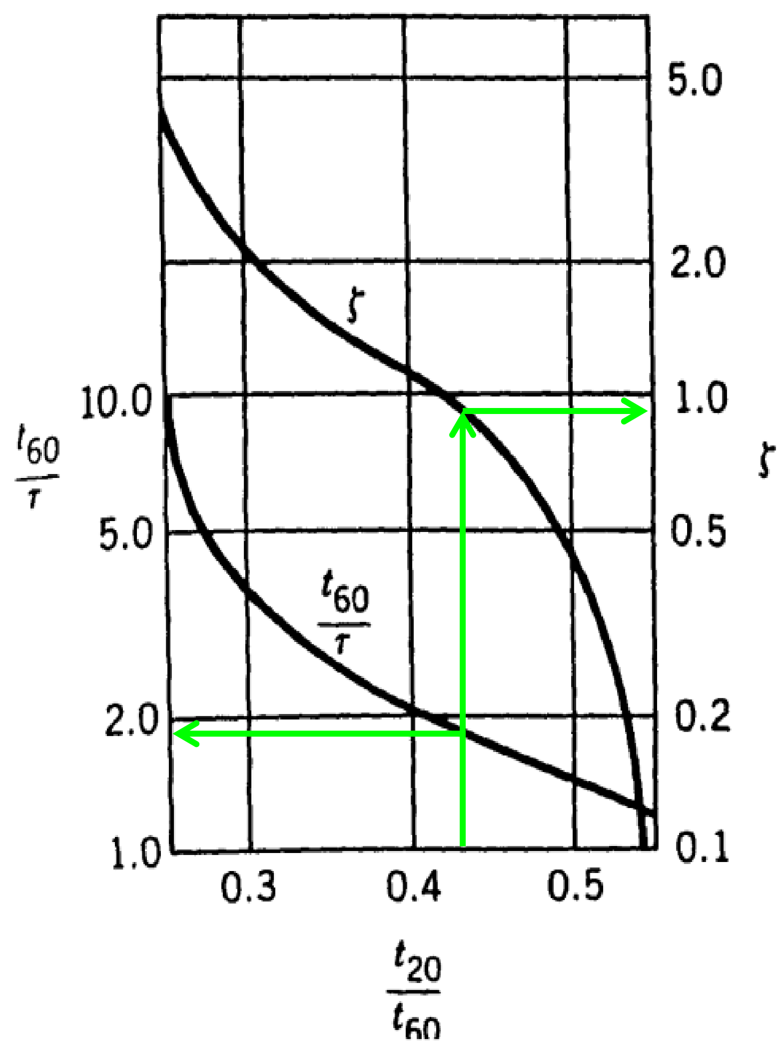
Second-order Model

- **Two limiting cases:**
  - $\tau_1/\tau_2 = 0$, where the system becomes first order, and,
  - $\tau_1/\tau_2 = 1$, the critically damped case ($\zeta = 1$)
- **Determine t_{20} and t_{60} from the step response.**
- **Find ζ and t_{60}/τ from Figure 14.**
- **Find t_{60}/τ from Figure 14 and then calculate τ (since t_{60} is known).**

Second-order Model



Second-order Model



Second Order plus Dead Time

- **Assumed model:**

$$G(s) = \frac{Ke^{-\theta s}}{\tau^2 s^2 + 2\zeta\tau s + 1}$$

If the original process transfer function contains a time delay

$$t = t' - \theta$$

Pergamon

Chemical Engineering Science, Vol. 51, No. 7, pp. 1149–1155, 1996

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ESTIMATING SECOND-ORDER DEAD TIME PARAMETERS FROM UNDERDAMPED PROCESS TRANSIENTS

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(*First received* 19 *August* 1994; *revised manuscript received* 5 *September* 1995; *accepted* 26 *September* 1995)

Abstract—Two simple methods for determining second-order dead time model parameters from underdamped process transients are presented. One of the methods relies on three characteristic points of the oscillatory step response curve. These three points attempt to minimize the integral of absolute error between process and model responses. The other method is based on just two points of the step response. Illustrative examples show that the proposed techniques allow rapid and reliable estimate of parameters.

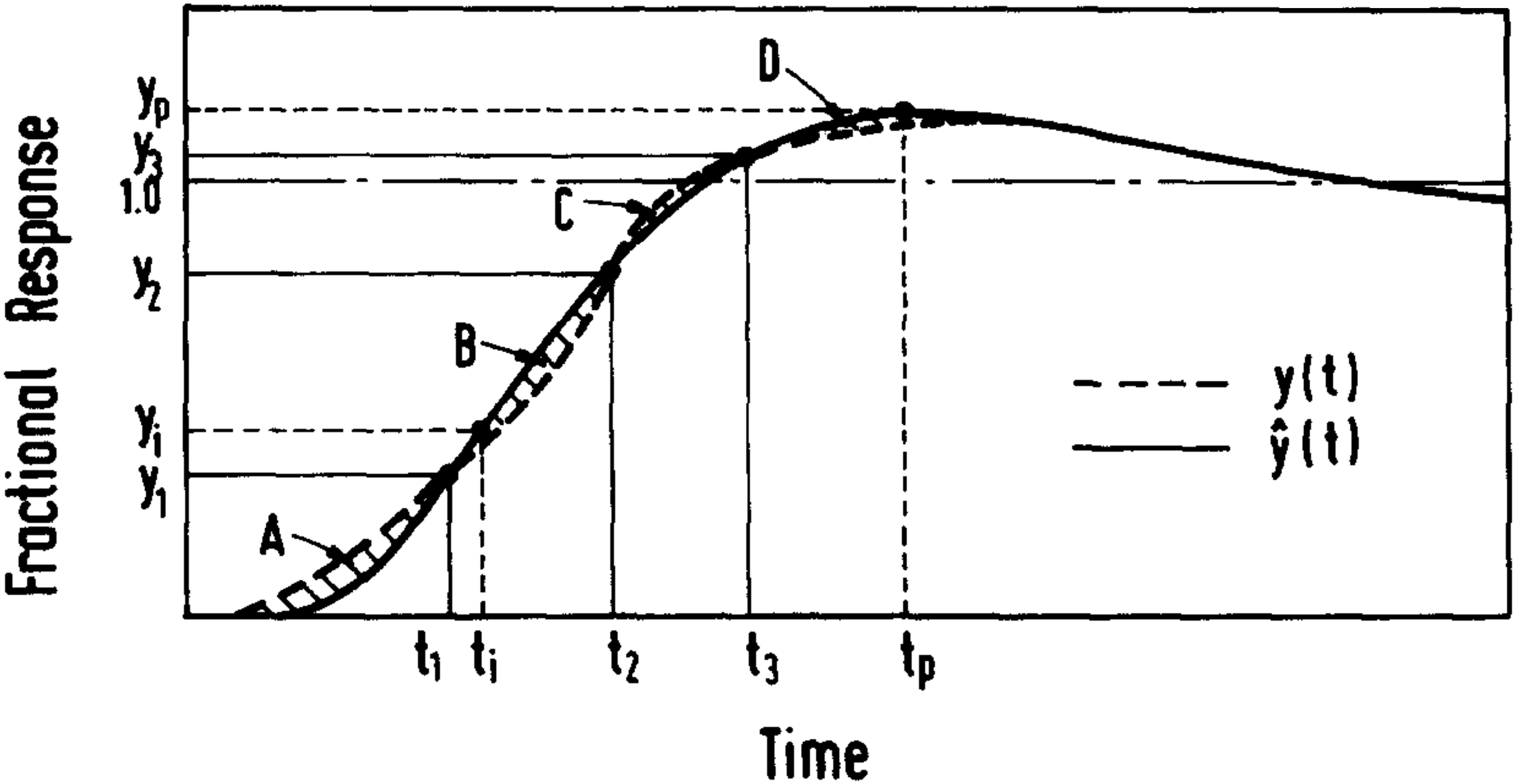


Fig. 1. Underdamped process response and second order dead time approximation.

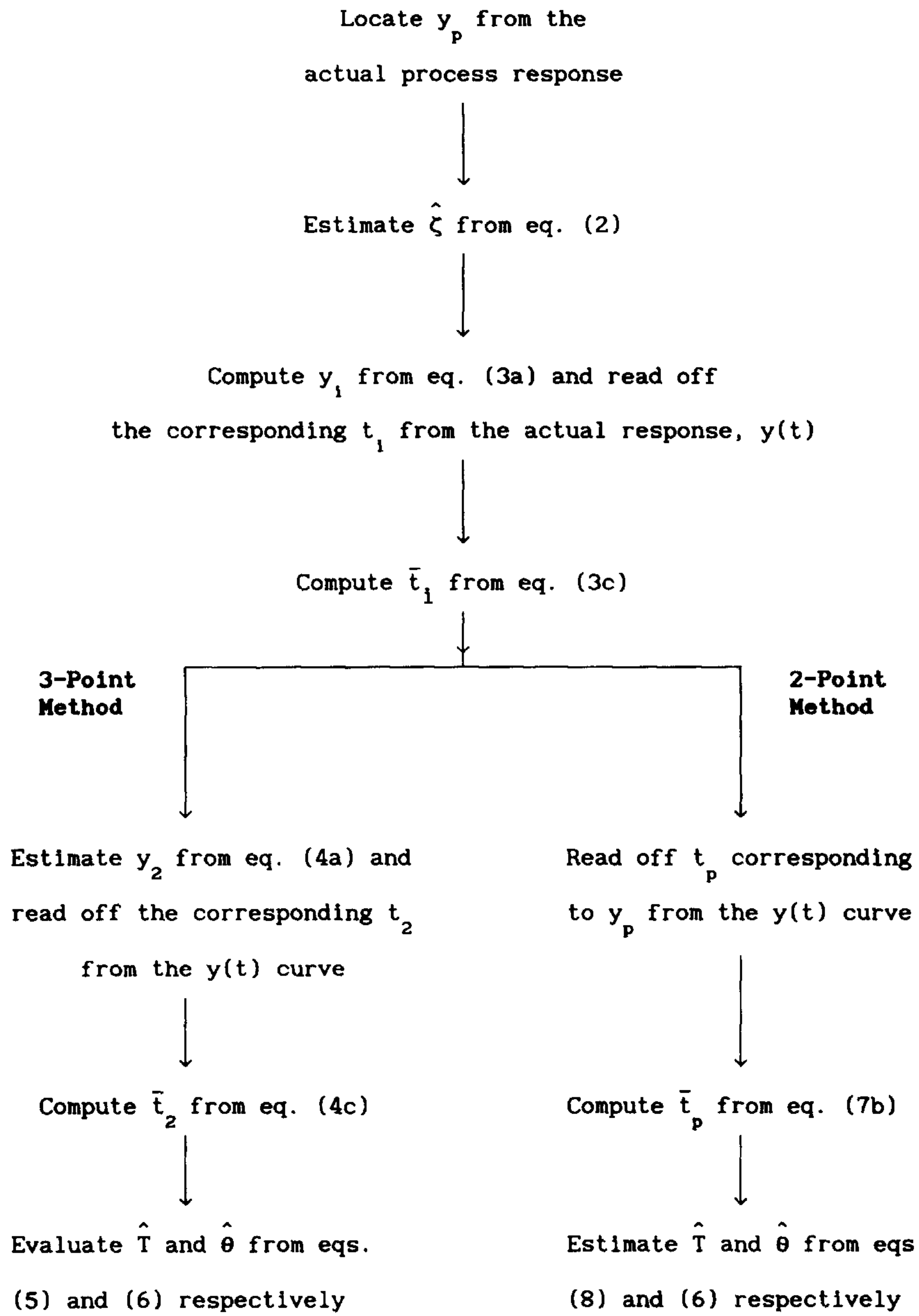


Fig. 3. Steps in the application of parameter estimation methods.

Ind. Eng. Chem. Res. **1994,** *33,* 174–176

Estimation of the Underdamped Second-Order Parameters from the System Transient

Chi-Tsung Huang* **and Chin-Jui Chou**

Department of Chemical Engineering, Tunghai University, Taichung 40704, Taiwan, ROC

A simple calculation method was presented in this study for estimating the parameters of the underdamped second-order-plus-dead-time model from the system transient. Several estimation techniques without graphic aid or computer searching were recommended on the basis of the value of the maximum overshoot. The model parameters were estimated in the range of $0 < \xi < 1$ using only a minimal number of data points along the step-response curve. This method was confirmed by the observed results as being both more reliable and easier to apply than currently available approaches for model parameter estimates.

$$\zeta = \left[\frac{\ln^2(y_p - 1)}{\pi^2 + \ln^2(y_p - 1)} \right]^{\frac{1}{2}}$$

- **According to the time response of 2nd order system,**

$$y_i = 1 - \frac{1}{\sqrt{1-\zeta^2}} \exp\left(-\frac{\zeta}{\sqrt{1-\zeta^2}} \tan^{-1} \frac{\sqrt{1-\zeta^2}}{\zeta} \right)$$

$$\sin\left(2 \tan^{-1} \frac{\sqrt{1-\zeta^2}}{\zeta} \right)$$

- **Find corresponding t_i from the time response, then calculate,**

$$\bar{t}_i = \frac{1}{\sqrt{1-\zeta^2}} \tan^{-1} \frac{\sqrt{1-\zeta^2}}{\zeta}$$

- **Finding y_2 according to**

$$y_2 = 1.8277 - 1.7652\zeta + 0.6188\zeta^2$$

- **Find corresponding t_2 from the time response, then calculate,**

$$\bar{t}_2 = 3.4752 - 1.3702\zeta + 0.1930\zeta^2$$

- **Find τ, θ using,**

$$\bar{t}_i = \left(t_i - \theta\right)/\tau$$
$$\bar{t}_2 = \left(t_2 - \theta\right)/\tau$$

Modeling Second-order Through Least Square Fit

- **For unit step input**

$$G(s) = \frac{C(s)}{R(s)} = \frac{C(s)}{\frac{1}{s}} = sC(s)$$

- **Assume *c*(*t*) takes the form,**

$$c(t) = c_{ss} + K_1 e^{-at} + K_2 e^{-bt} + \cdots$$

where c_{ss} is the final-value of *c*(*t*)

Table 4.1. Transient Response of Eq. (4.51) to a Unit Step Input to Obtain the Theoretical Value of $c(t)$, the Model Fit Data $\hat{c}(t)$, and the Error between the Theoretical Value of $c(t)$ and the Model Fit Data

Time (sec)	$c(t)$	$\hat{c}(t)$ (Model fit)	error $= c(t)-$fit of $\hat{c}(t)$
0	0	0	0
0.2000	0.1219	0.3994	−0.2775
0.4000	0.3374	0.6393	−0.3019
0.6000	0.5372	0.7833	−0.2462
0.8000	0.6916	0.8699	−0.1783
1.0000	0.8009	0.9218	−0.1210
1.2000	0.8743	0.9531	−0.0787
1.4000	0.9220	0.9718	−0.0498
1.6000	0.9523	0.9831	−0.0308
1.8000	0.9711	0.9898	−0.0187
2.0000	0.9826	0.9939	−0.0112
2.2000	0.9897	0.9963	−0.0067
2.4000	0.9939	0.9978	−0.0039
2.6000	0.9964	0.9987	−0.0023
2.8000	0.9979	0.9992	−0.0013
3.0000	0.9988	0.9995	−0.0008
3.2000	0.9993	0.9997	−0.0004
3.4000	0.9996	0.9998	−0.0002
3.6000	0.9998	0.9999	−0.0001
3.8000	0.9999	0.9999	−0.0001
4.0000	0.9999	1.0000	0.0000
4.2000	1.0000	1.0000	0.0000
4.4000	1.0000	1.0000	0.0000
4.6000	1.0000	1.0000	0.0000
4.8000	1.0000	1.0000	0.0000
5.0000	1.0000	1.0000	0.0000

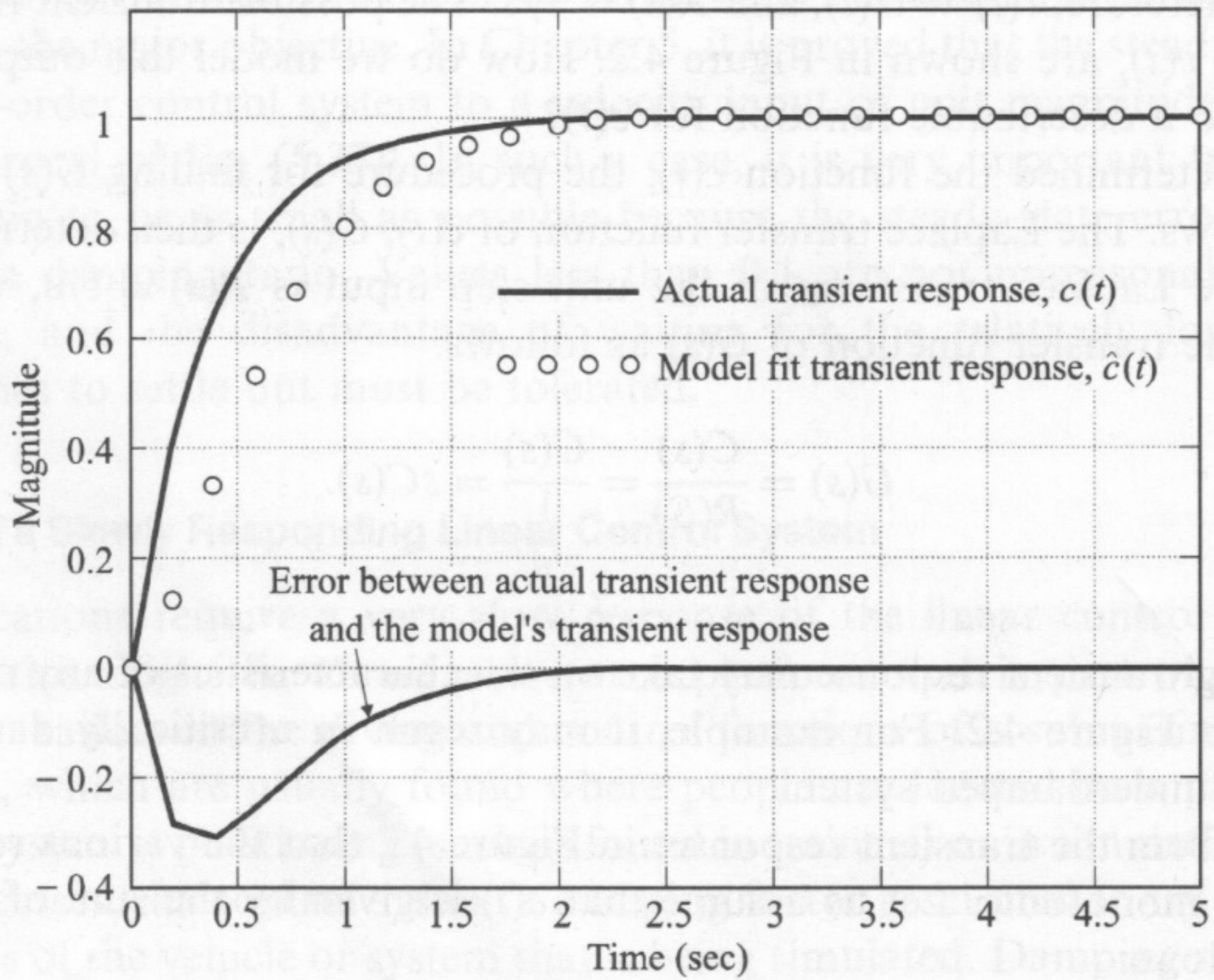


Figure 4.10 Transient response of the control system whose transfer function is given by Eq. (4.51) to a unit step input, and a model fit $\hat{c}(t)$.

Modeling Second-order Through Least Square Fit

- **Step 1: Least square fit first term**

$$c(t) - c_{ss} \approx K_1 e^{-at}$$

$$\log\left(c(t) - c_{ss}\right) \approx \log K_1 - at \log e$$
$$\approx \log K_1 - 0.4343at$$

The intercept is $\log K_1$

The slope is $0.4343a$

Modeling Second-order Through Least Square Fit

- **Step 2: Subtract the line fitted from the experimental data**

$$\log\left(c(t)-c_{ss}\right)-\log\left(K_1 e^{-at}\right)\approx \log K_2 - 0.4343bt$$

The intercept is $\log K_2$

The slope is $0.4343b$

Modeling Second-order Through Least Square Fit

- **Step 3: Adjustment to have *c*(0) = 0,**

$$adjustment = -\frac{1 - K_1 - K_1}{2} = ad$$

  - **Let**

$$K_1^{'} = K_1 + ad$$

$$K_2^{'} = K_2 + ad$$

  - **Now we have,**

$$c(t) = c_{ss} + K_1^{'} e^{-at} + K_2^{'} e^{-bt}$$

Time Responses Using State Variable Method

- **For non zero second order system,**

$$\frac{C(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

- **Divide s^2 on both numerator and denominator,**

$$\frac{C(s)}{R(s)} = \frac{\omega_n^2 s^{-2}}{(s^2 + 2\zeta\omega_n s + \omega_n^2)s^{-2}}$$

$$= \frac{\omega_n^2 s^{-2}}{1 + 2\zeta\omega_n s^{-1} + \omega_n^2 s^{-2}}$$

Time Responses Using State Variable Method

- **Define,**

$$E(s) = \frac{R(s)}{1 + 2\zeta\omega_n s^{-1} + \omega_n^2 s^{-2}}$$

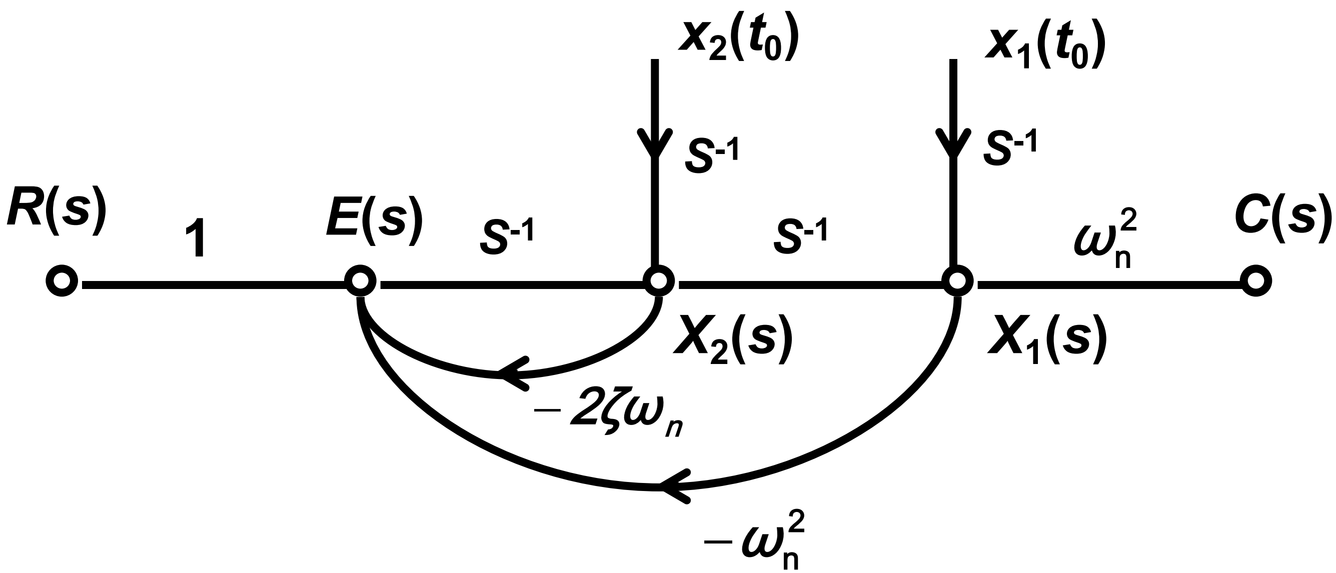
- **Therefore,**

$$C(s) = \omega_n^2 s^{-2} E(s)$$

$$E(s) = R(s) - 2\zeta\omega_n s^{-1} E(s) + \omega_n^2 s^{-2} E(s)$$

Time Responses Using State Variable Method

The state-variable signal-flow graph,



- Example

$$\ddot{c}(t) + 4\dot{c}(t) + 3c(t) = r(t)$$

- Laplace transform,

$$\frac{C(s)}{R(s)} = \frac{1}{s^2 + 4s + 3}$$

$$= \frac{s^{-2}}{1 + 4s^{-1} + 3s^{-2}}$$

- and

$$C(s) = s^{-2}E(s)$$

$$E(s) = \frac{R(s)}{1 + 4s^{-1} + 3s^{-2}}$$

$$E(s) = R(s) - 4s^{-1}E(s) - 3s^{-2}E(s)$$

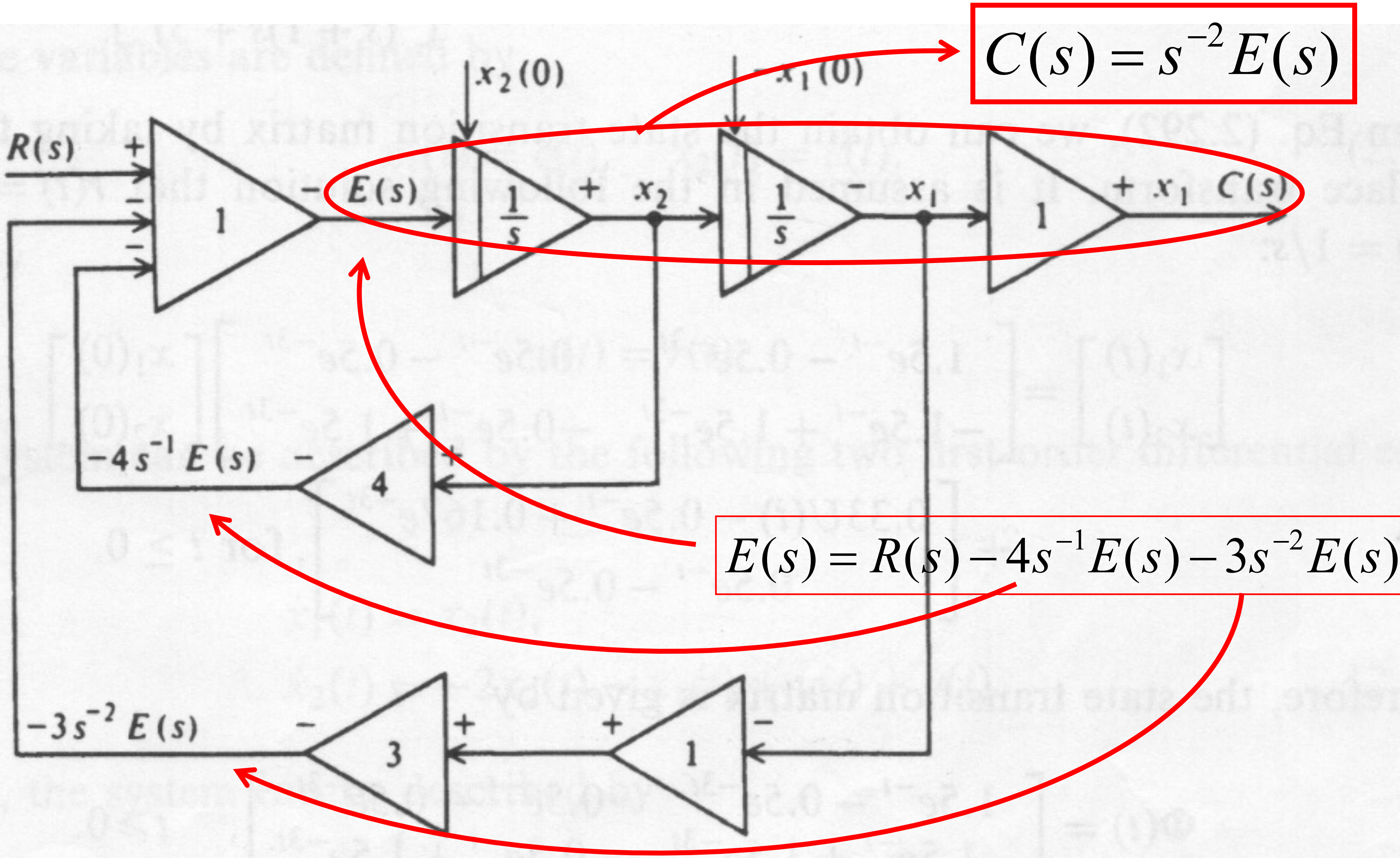


Figure 2.39 State-variable diagram for system where $C(s)/R(s) = 1/(s^2 + 4s + 3)$.

Quiz Answer